

Pontryagin Approximations for Optimal Design of Elastic Structures



Jesper Carlsson
NADA, KTH
jesperc@nada.kth.se

Collaborators: Anders Szepessy, Mattias Sandberg

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Optimal Design

A typical optimal design problem

$$\inf_{\rho:\Omega\rightarrow\{0,1\}} l(u), \quad a_\rho(u, v) = l(v), \quad \forall v \in V, \quad \int_{\Omega} \rho dx = C,$$

with compliance

$$l(u) \equiv \int_{\Omega} f_b \cdot u dx + \int_{\Gamma_N} f_s \cdot u ds,$$

and bilinear energy functional

$$a_\rho(u, v) \equiv \int_{\Omega} \rho \varepsilon_{ij}(u) E_{ijkl} \varepsilon_{kl}(v) dx.$$

An alternative formulation

$$\inf_{\rho:\Omega\rightarrow\{0,1\}} \left(l(u) + \eta \int_{\Omega} \rho dx \right), \quad a_\rho(u, v) = l(v), \quad \forall v \in V.$$

Problem Optimal design problems are typically ill-posed i.e. no existence of solution.

Cure To relax the admissible set of controls \mathcal{A} , $\rho \in \mathcal{A}$.

Optimal design, continued

A harder inverse problem

$$\inf_{\rho} \int_{\Gamma} (u - u_{\text{given}})^2 ds$$
$$a_{\rho}(u, v) = l(v), \quad \forall v \in V.$$

Ill posed due to non-continuous dependence of error in measured data.

Hamilton-Jacobi-Bellman and the Pontryagin Principle

$$\inf_{\alpha \in \mathcal{A}} \left\{ g(X_T) + \int_0^T h(X_t, \alpha_t) dt \right\}, \quad X'_t = f(X_t, \alpha_t), \quad X(0) = X_0$$

Value function

$$u(x, t) = \inf_{\alpha \in \mathcal{A}, X(t)=x} \int_t^T h(X_s, \alpha_s) ds + g(X_T)$$

solution to the HJB-equation

$$u_t + \overbrace{\min_{\alpha \in \mathcal{A}} \{ u_x \cdot f(x, \alpha) + h(x, \alpha) \}}^{H(u_x, x)} = 0, \quad u(x, T) = g(x)$$

Differentiation along optimal paths $\alpha_t, X_t, \lambda_t \equiv u_x(X_t, t)$ gives Pontryagin's Principle

$$\lambda'_t = -\lambda_t f_X(X_t, \alpha_t) + h_X(X_t, \alpha_t), \quad \lambda(T) = g'(X_T)$$

Also

$$\alpha_t = \operatorname{argmin}_{a \in \mathcal{A}} \{ \lambda_t \cdot f(X_t, a) + h(X_t, a) \}$$

Assume H, f, h, g differentiable, $\lambda \in C^1$.

Lagrange principle

$$\begin{aligned} X_t' &= H_\lambda(\lambda_t, X_t) \\ -\lambda_t' &= H_X(\lambda_t, X_t) \end{aligned}$$

with control determined by Pontryagin principle

$$\alpha_t = \operatorname{argmin}_{a \in \mathcal{A}} \{ \lambda_t \cdot f(X_t, a) + h(X_t, a) \}$$

Two reasons for non-smooth control:

1. Only Lipschitz continuous Hamiltonian
2. Backward characteristic paths $X(t)$ may collide

Remedy for 1: construct a \mathcal{C}^2 concave approximation H^δ of the Hamiltonian H .
Error estimate [Sandberg, Szepeszy 2005]:

$$\|\bar{u} - u\|_{L^\infty(\mathbb{R}^d \times \mathbb{R}_+)} = \mathcal{O}(\delta)$$

Concave Maximization in Electric Conduction

Minimize power-loss in conductive medium [Pironneau 1984]

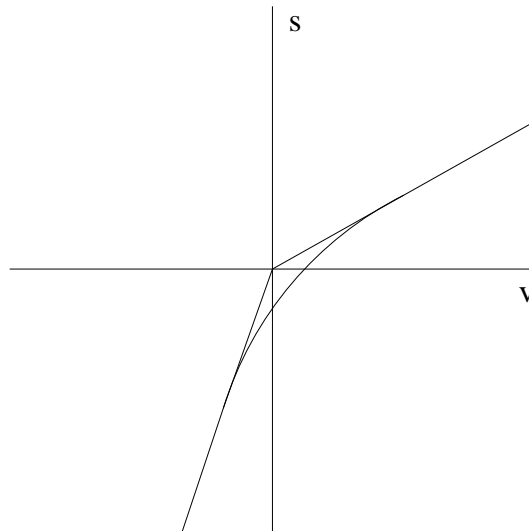
$$\min_{\sigma} \left(\int_{\partial\Omega} q\varphi ds + \eta \int_{\Omega} \sigma dx \right) \quad \operatorname{div}(\sigma \nabla \varphi) = 0, \quad x \in \Omega \quad \sigma \frac{\partial \varphi}{\partial n} \Big|_{\partial\Omega} = q$$

Lagrangian

$$\int_{\Omega} \sigma \underbrace{(\eta - \nabla \varphi \cdot \nabla \lambda)}_v dx + \int_{\partial\Omega} q(\varphi + \lambda) ds$$

Hamiltonian

$$H = \min_{\sigma} \int_{\Omega} \sigma v dx + \int_{\partial\Omega} q(\varphi + \lambda) ds = \int_{\Omega} \underbrace{\min_{\sigma} \sigma v}_{s(v)} dx + \int_{\partial\Omega} q(\varphi + \lambda) ds$$



Concave regularization

$$H^\delta = \int_{\Omega} s_\delta(\eta - \nabla \varphi \cdot \nabla \lambda) dx + \int_{\partial\Omega} q(\varphi + \lambda) ds,$$

By symmetry $\lambda = \varphi$ the Hamiltonian system reduces to

$$\int_{\Omega} s'_\delta(\eta - |\nabla \varphi|^2) \nabla \varphi \cdot \nabla w dx = \int_{\partial\Omega} q w ds$$

or

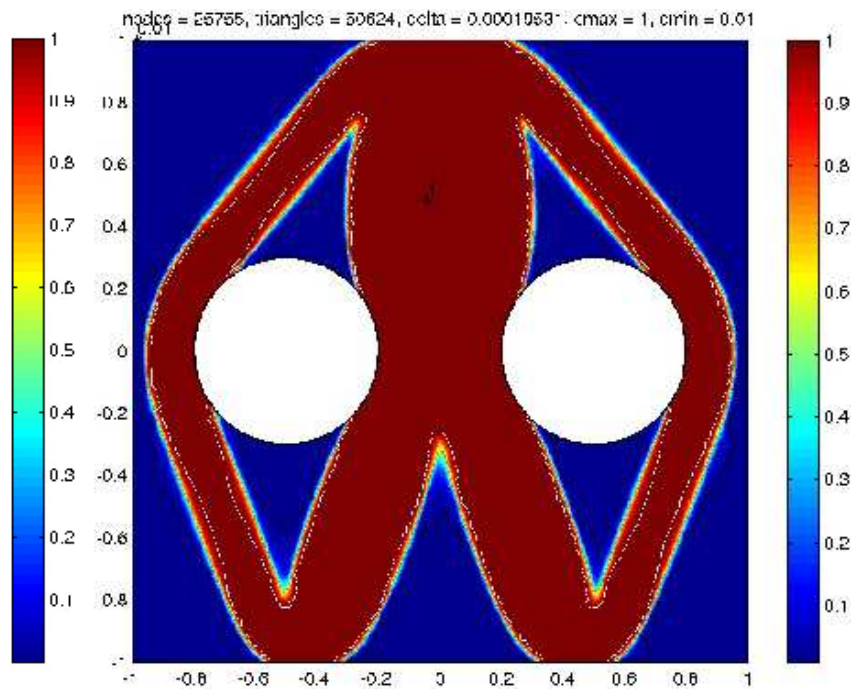
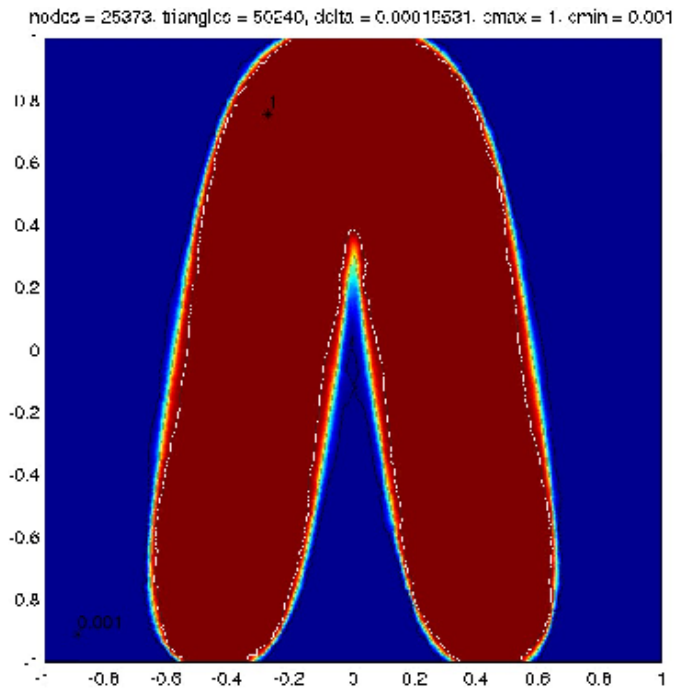
$$\operatorname{div}(s'_\delta(\eta - |\nabla \varphi|^2) \nabla \varphi(x)) = 0, \quad x \in \Omega$$

$$s'_\delta \frac{\partial \varphi}{\partial n} \Big|_{\partial\Omega} = q,$$

Concave maximization problem: $\varphi \in V$ is the unique maximizer of

$$H^\delta(\varphi) = \int_{\Omega} s_\delta(\eta - |\nabla \varphi(x)|^2) dx + 2 \int_{\partial\Omega} q \varphi ds.$$

Numerical Examples of Electric Conduction



Optimal Design of an Elastic Structure

Lagrangian for compliance minimization

$$l(u) + l(\lambda) + \int_{\Omega} \rho \left(\underbrace{\eta - \varepsilon_{ij}(u) E_{ijkl} \varepsilon_{kl}(\lambda)}_v \right) dx,$$

Hamiltonian

$$H = l(u) + l(\lambda) + \int_{\Omega} \underbrace{\min_{\rho} \rho v}_{s(v)} dx.$$

Regularization gives Hamiltonian system which by symmetry $u = \lambda$ reduces to

$$\int_{\Omega} s'_{\delta} \left(\eta - \varepsilon_{ij}(u) E_{ijkl} \varepsilon_{kl}(u) \right) \varepsilon_{ij}(u) E_{ijkl} \varepsilon_{kl}(v) dx = l(v)$$

Concave maximization problem: u is the unique maximizer of

$$H^{\delta} = 2l(u) + \int_{\Omega} s_{\delta} \left(\eta - \varepsilon_{ij}(u) E_{ijkl} \varepsilon_{kl}(u) \right) dx.$$

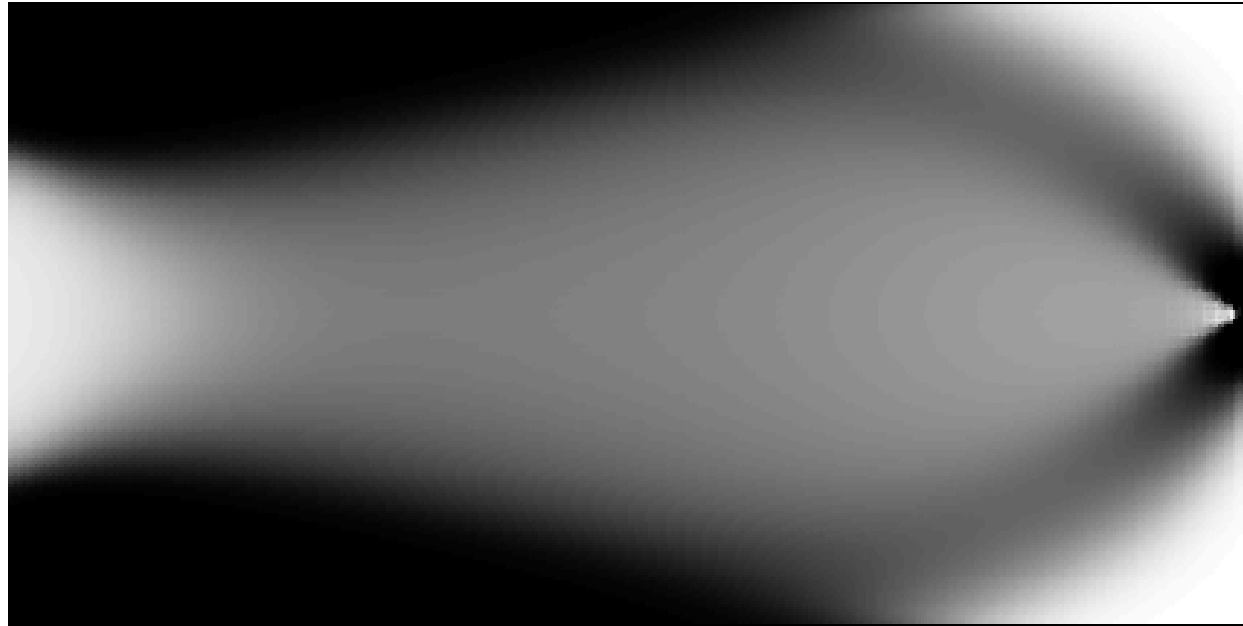


Figure 1: Plot of s'_δ as approximation of $\rho \in [0.001, 1]$. Compliance = 0.45.

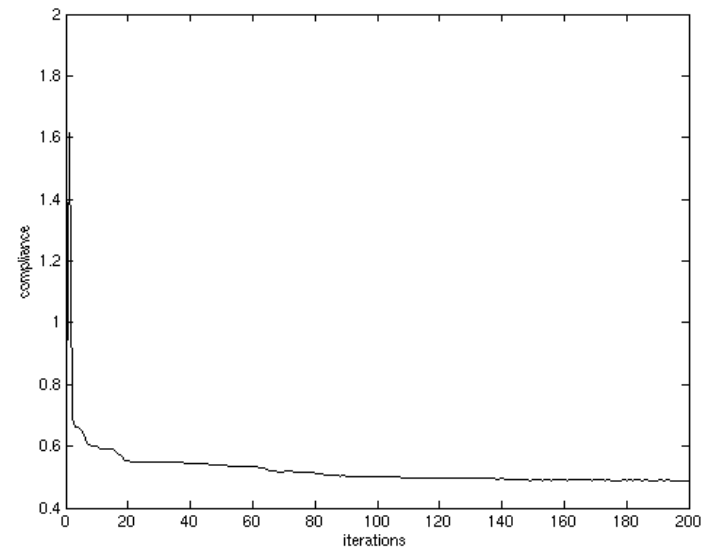
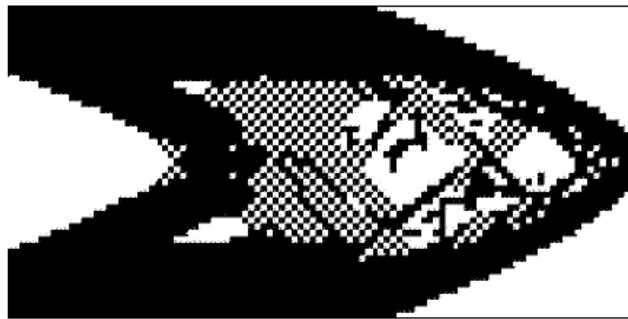
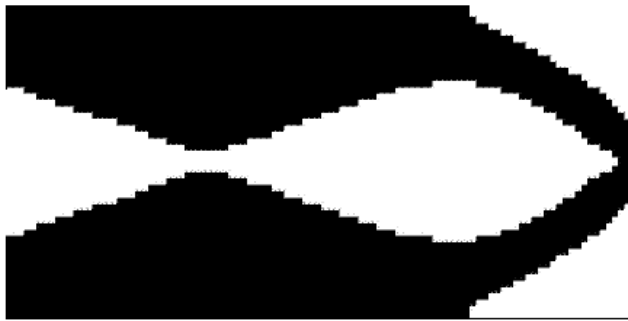


Figure 2: Plot of the density $\rho \in \{0.001, 1\}$ after 1, 5 and 200 iterations.

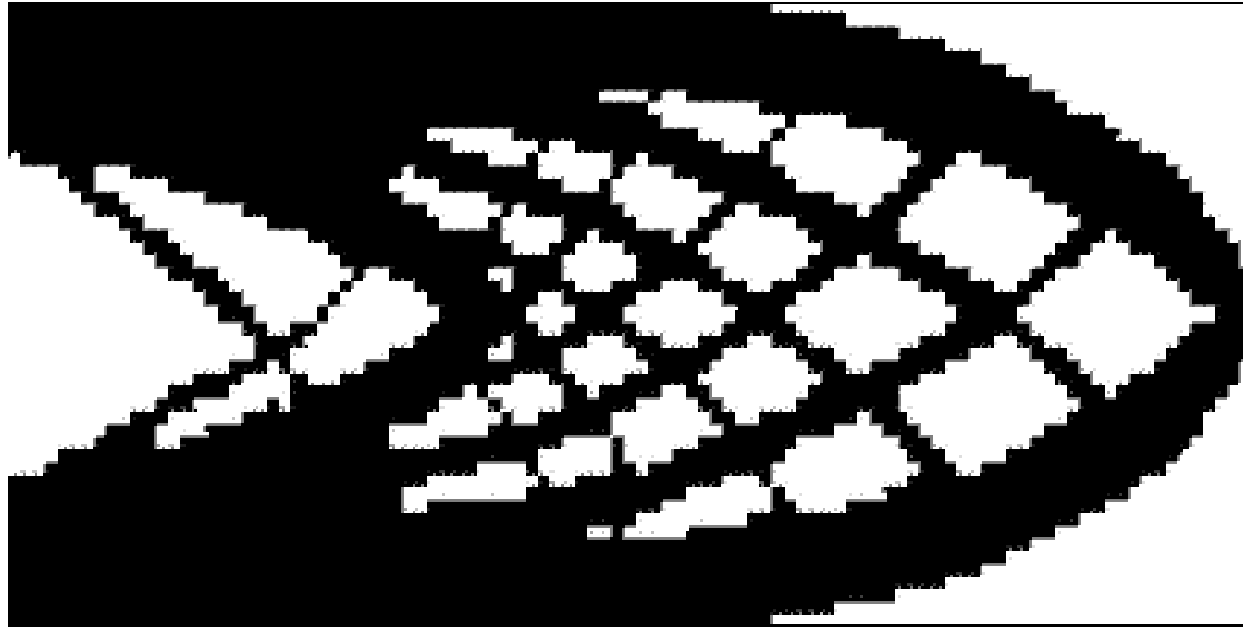


Figure 3: 10 iterations when only removing material. Compliance = 0.51.

References

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