Comsol Laboration
Design of Bourgogne Organ
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1 Background

CSC

The task is to determine the frequency of the sound obtained by blowing across the mouth of a partially filled standard Bourgogne bottle, and to select the liquid levels to make a properly tuned bottle organ. The rotationally symmetric geometry is defined by the bottom radius R, also the radius of the spherical shoulder segment, the height H, the neck radius r and length h, the liquid level is x.



Figure 1: 2D Axis Symmetric Geometry of the Bourgogne bottle

2 Helmholtz Resonator Model

In the Swedish High-school national physics contest 1994 one learns that the contraption is a Helmholtz resonator, where the air in the bottleneck acts as a rigid body, and the (large) volume in the bottle itself acts as a spring. The test suggests the use of pV = const., i.e. assuming that the process is isothermal. This is erroneous and gives about 20% error, see below, so one should use instead γ =ratio of specific heats for air = 1.4,

$$\frac{dp}{dV} = -\gamma \frac{p}{V} \tag{1}$$

i.e. $pV^{\gamma} = const.$ One can deduce from this the lowest resonance frequency.

3 Analytical and Preparation Tasks

1. Q.1 You may assume that H = 3R, R = 3r, and volume = 3/4 litres, the temperature is 20° , and standard air pressure of 10^{5} Pa, at which conditions the density of air is $\rho = 1.273$ Kg/m³. Plot the frequency as function of x, $0 \le x \le H$

Hint: The air plug has mass $m = (\ldots)$ Kg and is accelerated by the pressure difference

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acting on its cross section area A. If it has velocity v, positive outward, then the volume rate of change of the air in the large volume V is $\frac{dV}{dt} = Av$ But $\frac{dp}{dt} = \frac{\partial p}{\partial V}\frac{dV}{dt}$ so we now have two first order equations for p and V from which the resonance frequency can be obtained (by linearization).

4 COMSOL Calculations

4.1 Eigenvalue computation

Now let us do this by eigenvalue computation in COMSOL. It follows from thermodynamics that air pressure deviations p from ambient pressure P are described by the wave equation,

$$p_{tt} = c^2 \Delta p \tag{2}$$

 $\frac{\partial p}{\partial n} = 0 \text{ at solid boundaries}$ p = 0 at the mouth

c is the adiabatic speed of sound, 340 m/s at the conditions above.

- 1. Q2 Plot the frequency as function of x, $0 \le x \le H$, in the same diagram as the curve in 1.
- Q3 Comment on the differences between the Helmholtz resonator results and the(probably more accurate) COMSOL results.
 READ QUESTION 3 BEFORE DOING THE CALCULATIONS!

4.2 Variation in x

The variation of x is conceptually most easily treated by using the parametrized geometry Module. An option is to include the pressure waves in the liquid so the liquid level becomes a parameter which can be changed without changing the geometry. Here is how:

4.2.1 Liquid

The liquid is almost incompressible and the correct model is

 $(E)^{-1}p_{tt} = \nabla \cdot \left(\frac{1}{\rho}\nabla p\right)$

where E is the elastic modulus (N/m^2) and ρ is the density $(1000 \text{ kg}/m^3)$. It is known that the sound speed in water is about 1500 m/s.

• Q.4 Deduce the value of E from this. Hint: With constant ρ and E we obtain $p_{tt} = E/\rho\Delta p$

4.2.2 Gas

The equation for the gas is

$$(c^2 \rho)^{-1} p_{tt} = \nabla \cdot \left(\frac{1}{\rho} \nabla p\right) \tag{3}$$

4.2.3 Interface conditions

For the whole model, p and $\frac{\frac{\partial p}{\partial n}}{\rho}$ must be continuous across the interface. This comes automatically with the FE formulation. Define ρ as

$$\rho(r,z) = Hs(z-x)\rho_{Gas} + (1 - Hs(z-x))\rho_{Liq}$$

where Hs(s) is a smoothed Heaviside function jumping from 0 to 1 at s = 0. A similar definition is made of the coefficient of p_{tt} (called e_a in COMSOL),

$$e_a(r,z) = Hs(z-x)\frac{1}{\rho_{Gas}c^2} + (1 - Hs(z-x))\frac{1}{E_{Liq}}$$

4.3 Heaviside Function

Hs jumps over a distance d, a parameter to the FLH2S function built into COMSOL. One suspects that d must be O(element size) so the jump occurs over a few elements lest the quadratures become inaccurate.

- Q5 Experiment with small d. Look at the pressure gradient near the interface. If it looks spiky d is too small.
- Q6 Run the computations. Compare a few with results obtained by changing the geometry.
- Q7 So armed with the tables, select the eight liquid levels.

5 COMSOL implementation

- 5.1 Mode
- 5.2 Geometry
- 5.3 Constants
- 5.4 Expressions
- 5.5 Solver Settings
- 5.6 Convergence Study

6 Appendix

Adiabatic relation between pressure p and Volume V

Assume that the process is adiabatic, i.e. no heat exchange with the outside. Then, for the volume in the bottle

0 = added heat = dQ = dE + pdV

where p = m/V R T, R = universal gas constant Assuming the gas to be calorically perfect, its internal energy per unit mass e depends only on temperature:

$$\mathbf{E} = \mathbf{m}\mathbf{e} = \mathbf{m} C_v \mathbf{T} = \mathbf{p} C_v \mathbf{V/R},$$

so

$$0 = C_v/R d(pV) + p dV = (C_v/R + 1) p dV + C_v/R V dp;$$

$$\frac{dp}{dV}_{dQ=0} = -(C_v + R)/C_v p/V = -\gamma p/V$$

where γ is 7/5 = 1.4, a value which can be deduced from the kinetic theory of gases for twoatomic gases such as air. The isothermal process has $\frac{dp}{dV_{dT=0}} = -p/V$ so the error is 40% which translates into an error of 20% in wave speed. Use the correct relation in problem 1.